

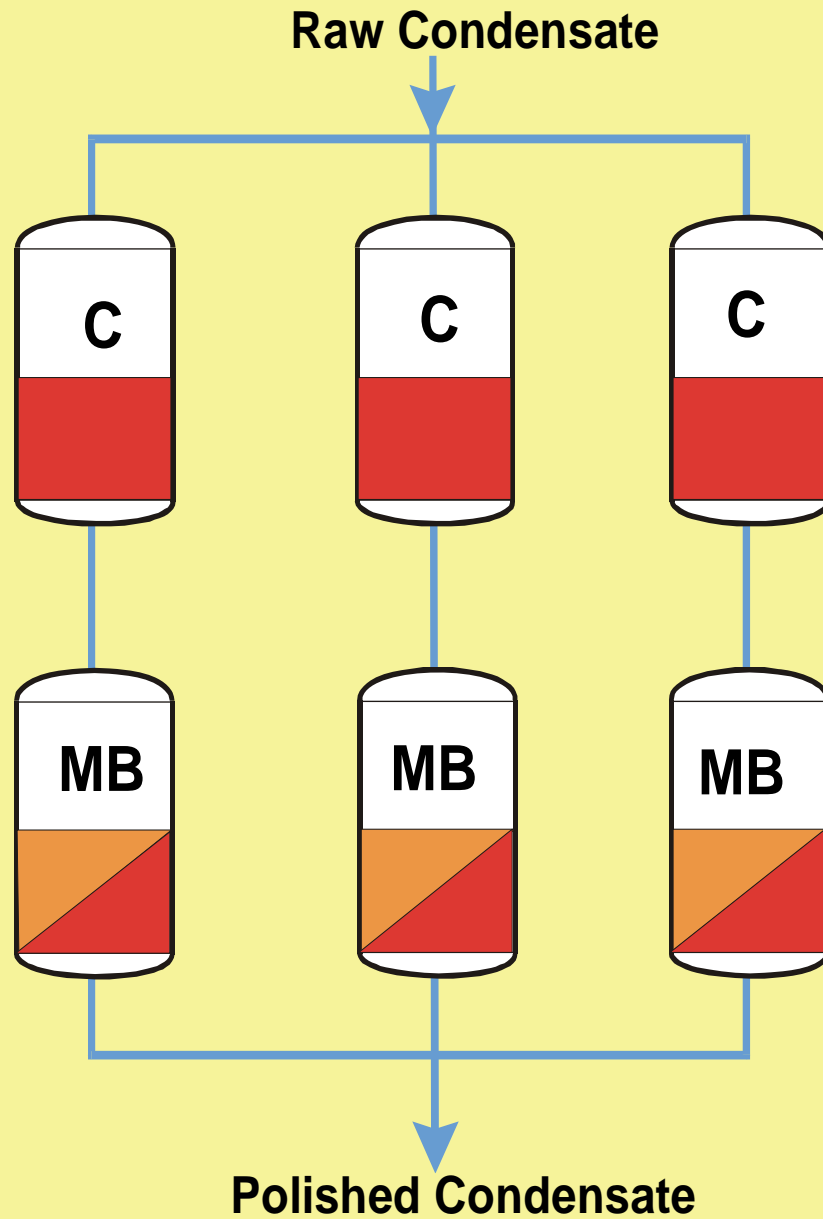
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**CONDENSATE POLISHING PLANT  
WITH SEPARATE BEDS  
EXCEEDS ALL EXPECTATIONS**

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# Traditional CPP



## C - MB

### Advantage

Continuous full flow operation

Reliable

High purity condensate

Good kinetic properties

– acidic conditions

### Disadvantage

Difficult automation

Leachables from cation resin

- reheater corrosion

- SCC in LP turbine

# New generation

## Target

Keep all the advantages

Reduce the disadvantages

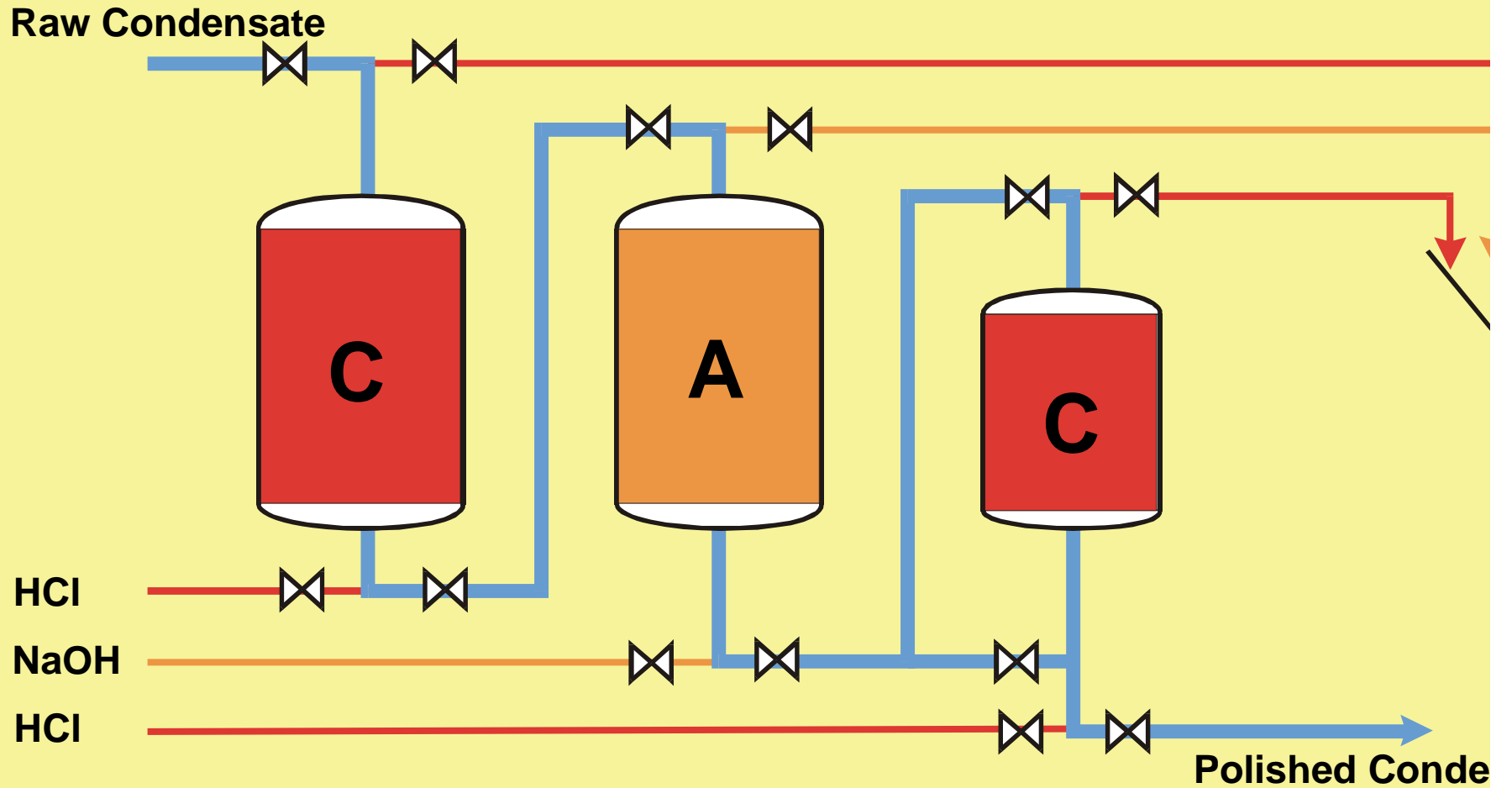
## Means

New concept - C – A – (C)

Resin choice

Operational efforts

# Counter current regenerated CPP



## Calculation of the leachables release

Assumption –  $C_{\text{trail}}$  by-passed > 90 % of the time  
-50 % of C leachables retained by A

C – MB      -42 % enter the cycle

C – A – (C)    -36 % enter the cycle

Calculated reduction at least      15 %

**Experience** –  $C_{\text{trail}}$  by-passed > 99 % of the time

Realised reduction at least      21 %

# Resin choice

OSA test –

All the resins were OK

Kinetic of anion resin (MTC) –

No difference

Leachables of cation resin –

Producer	Product	Unit SKV	Unit NJV
1	Sample A	7	-
2	Sample C	16	-
1	Supplied A	25	-
1	Sample B	-	23
2	Sample D	-	8
2	Supplied D	-	15



# Operational efforts

Initial leachables – Pre-treatment

Stand-by rinse – Daily rinse with 2 BV

Brine cleaning – After 5 years operation

# Operational experience

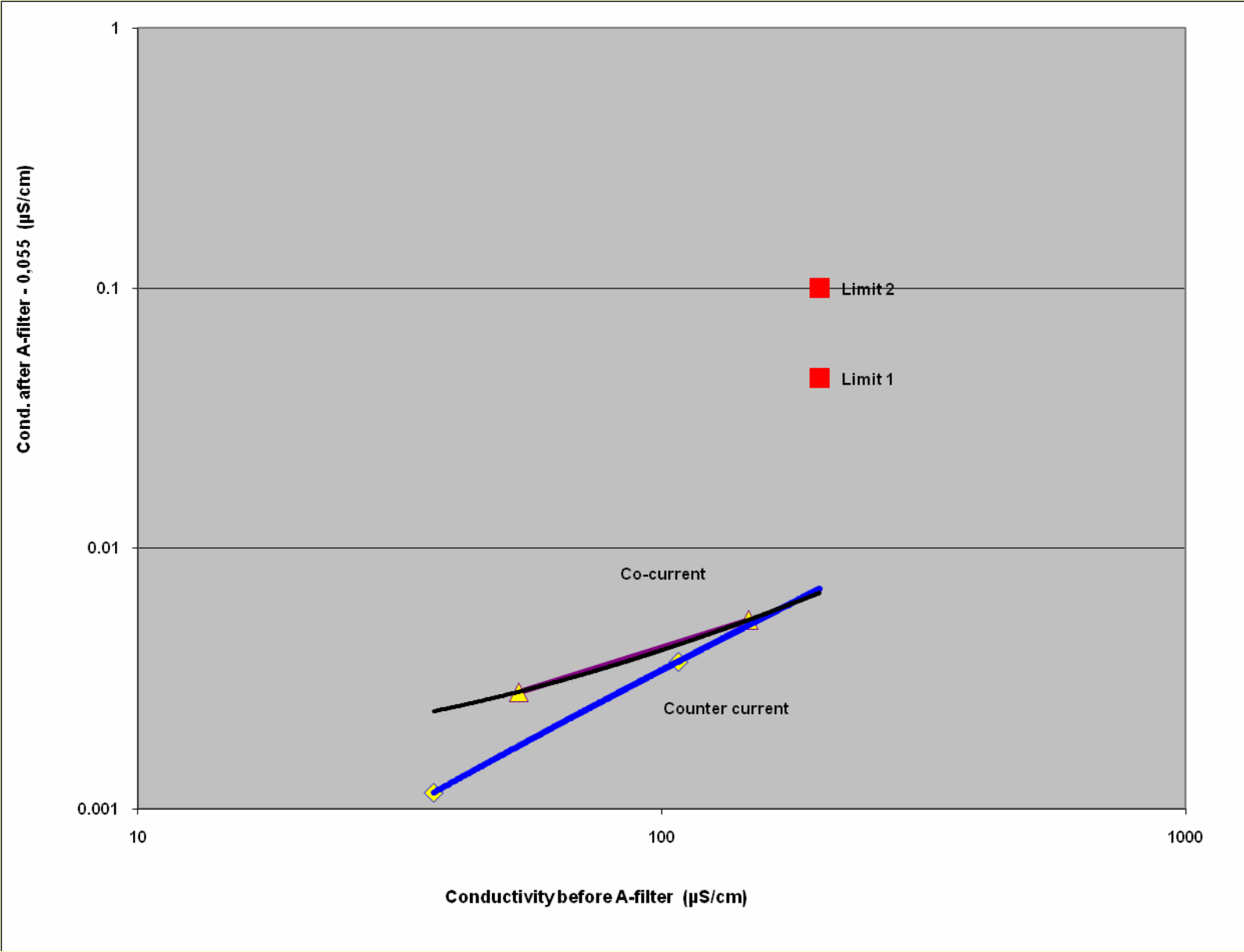
## Performance test

- Capacity  $C_{\text{lead}}$  resin – 1 & 1.1 eq/L
- Kinetic of A resin
- Ionic leakage - < 0.3  $\mu\text{g/L}$  typically
- Organic carbon leakage- <10  $\mu\text{g/L}$  typically

## Survey of 10 years operation

- Ionic leakage from  $C_{\text{lead}}$
- Ionic leakage from A - < 0.3  $\mu\text{g/L}$  typically

# Kinetic test of CPP



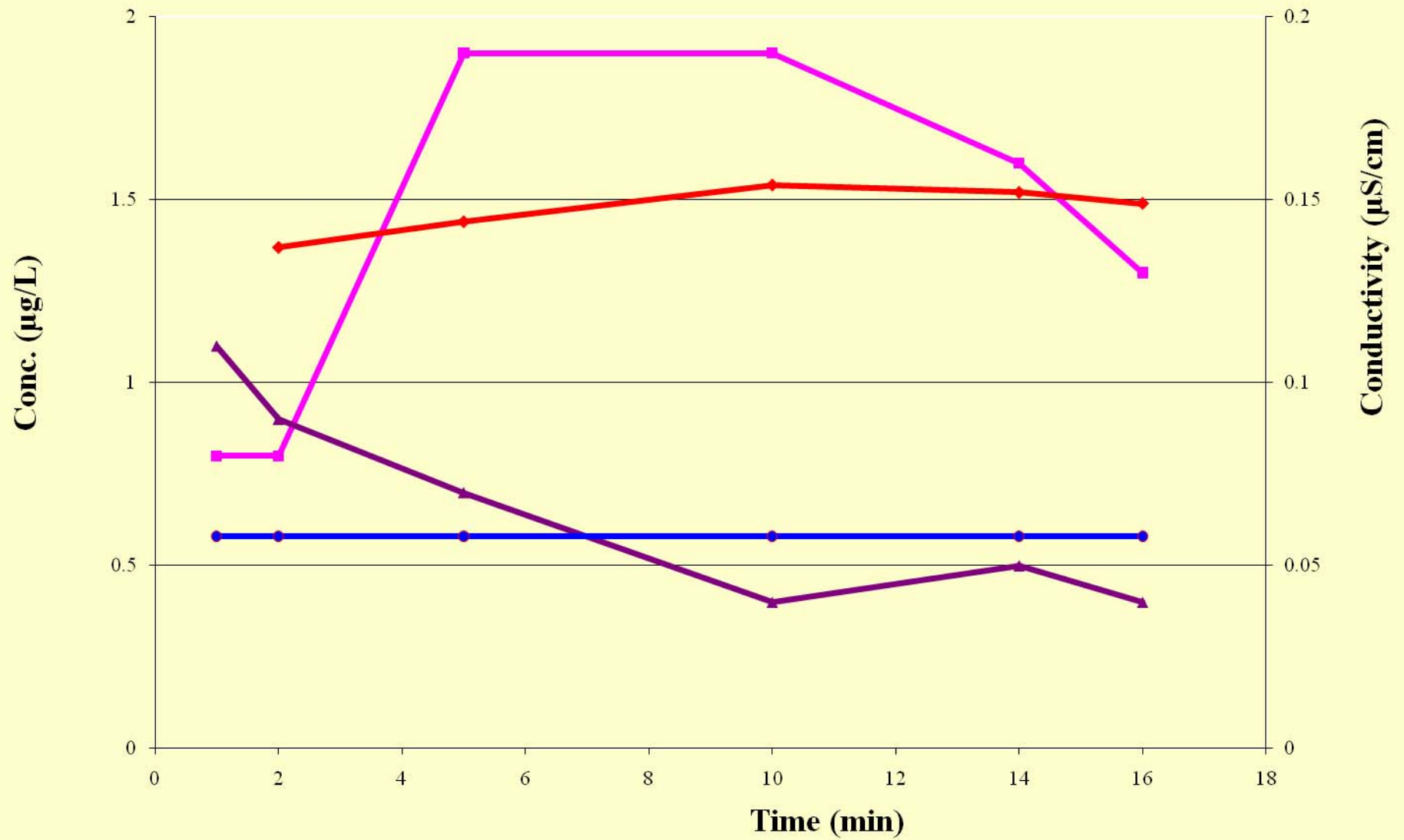
## Average leakage in the first year of operation

	Sample after No.	Co-flow regenerated			Reverse-flow Anion
		Lead Cation	Anion	Trail Cation	
		50	50	3	
<b>Conductivity</b>	$\mu\text{S cm}^{-1}$	<b>0.126</b>	<b>0.057</b>	<b>0.058</b>	<b>0.126</b>
<b>Fluoride</b>	$\mu\text{g L}^{-1}$	<b>0.4</b>	<b>0.1</b>	<b>0.1</b>	
<b>Acetate</b>	$\mu\text{g L}^{-1}$	<b>0.6</b>	<b>0.5</b>	<b>0.3</b>	<b>0.5</b>
<b>Format</b>	$\mu\text{g L}^{-1}$	<b>0.3</b>	<b>0.2</b>	<b>0.3</b>	<b>0.5</b>
<b>Chloride</b>	$\mu\text{g L}^{-1}$	<b>0.6</b>	<b>0.3</b>	<b>0.7</b>	<b>&lt; 0.1</b>
<b>Sulfate</b>	$\mu\text{g L}^{-1}$	<b>0.3</b>	<b>0.2</b>	<b>0.7</b>	<b>&lt; 0.1</b>
<b>Sodium</b>	$\mu\text{g L}^{-1}$	<b>0.2</b>	<b>0.1</b>	<b>0.1</b>	<b>0.3*</b>
<b>Ammonium</b>	$\mu\text{g L}^{-1}$	<b>3.8</b>	<b>3.3</b>	<b>0.5</b>	
<b>Magnesium</b>	$\mu\text{g L}^{-1}$	<b>0.1</b>	<b>0.0</b>	<b>0.0</b>	
<b>Calcium</b>	$\mu\text{g L}^{-1}$	<b>0.2</b>	<b>0.1</b>	<b>0.6</b>	

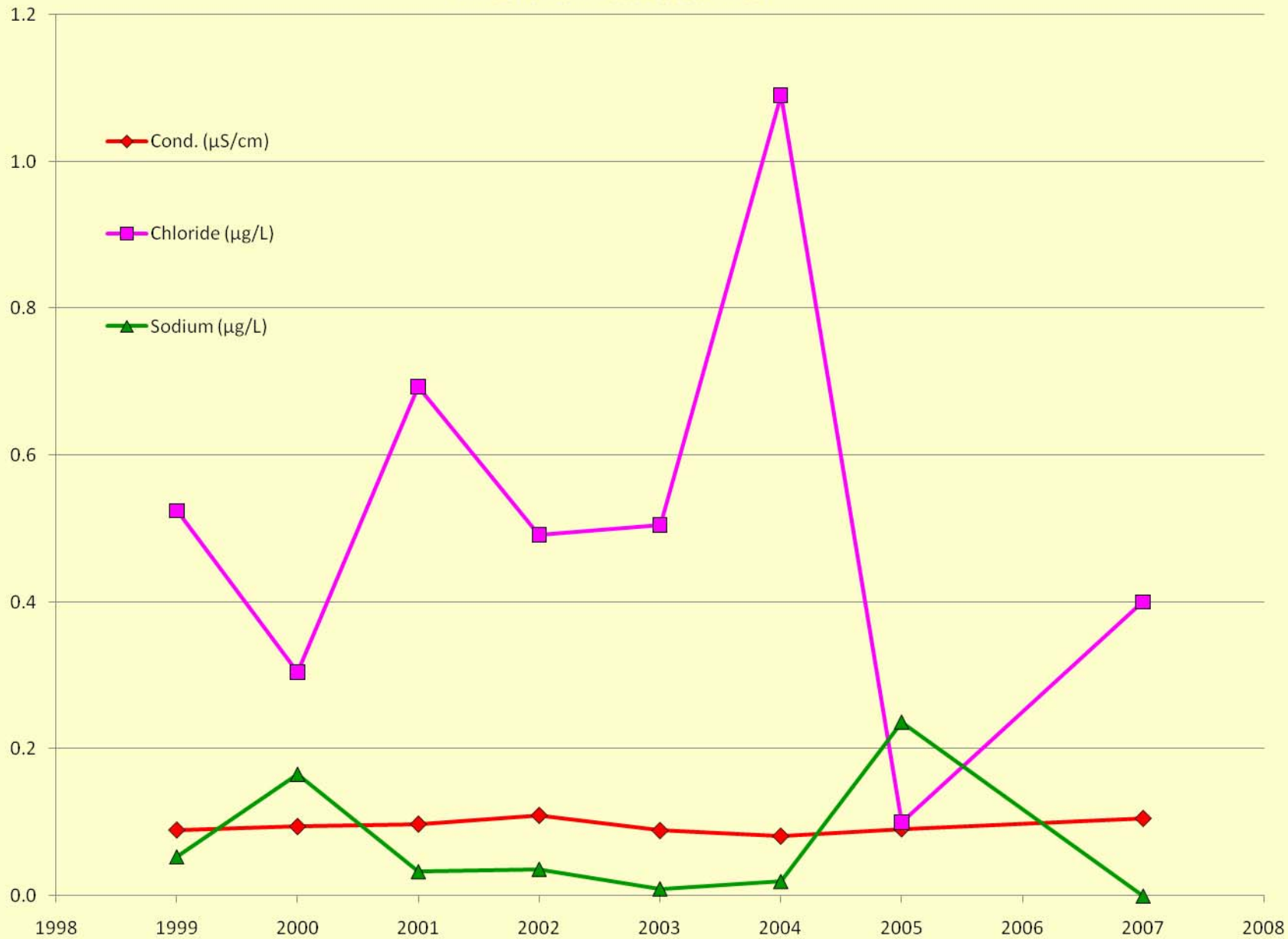
# Organics in condensate

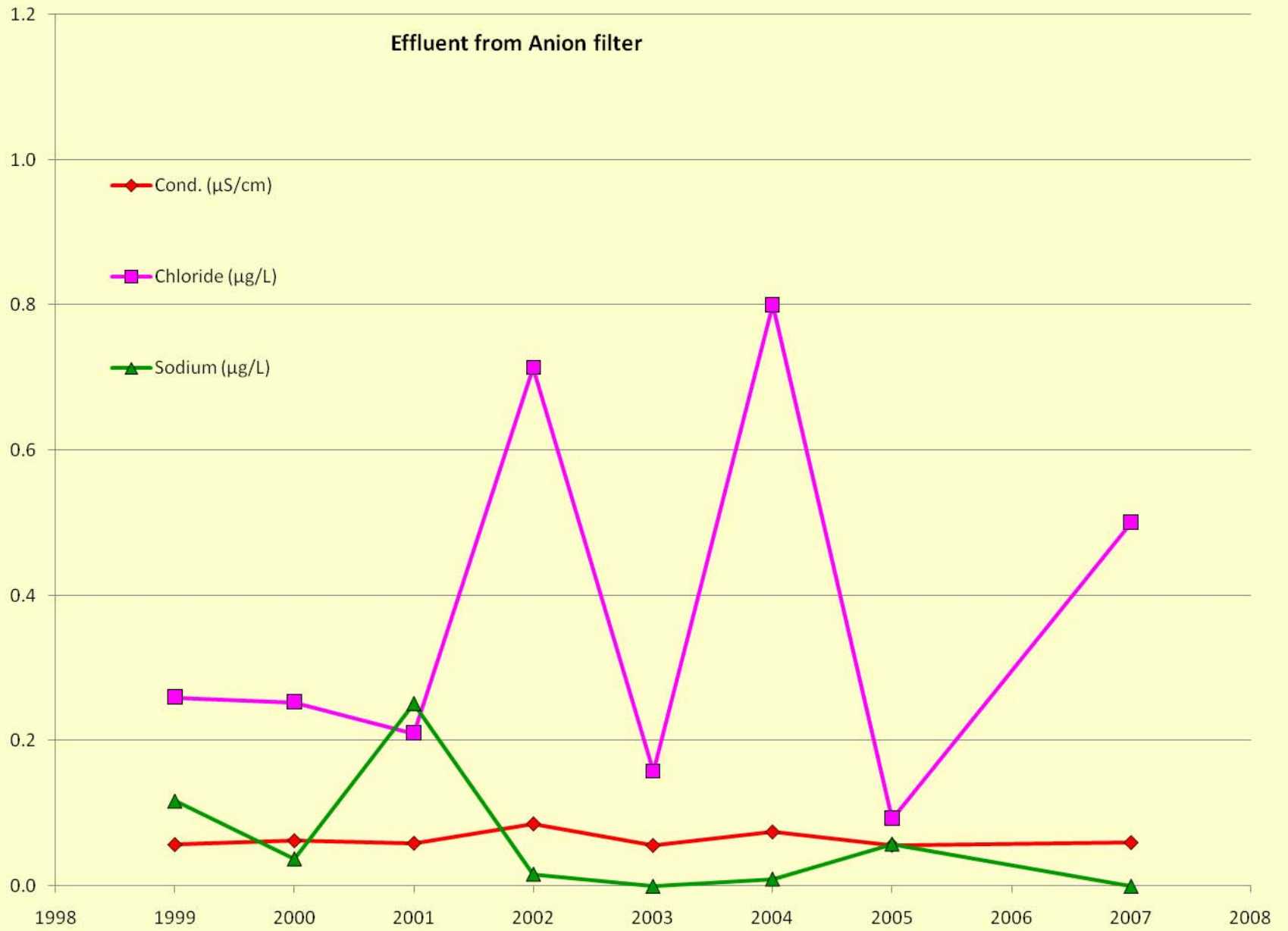
Time (min)	Volume (m <sup>3</sup> )	TOC (μg L <sup>-1</sup> )			
		Raw Cond.	After lead C	After A	After trail C
2	8	57	51	31	62
11	55		54	47	27
14	76	58	50	53	27
16	86	28	38	53	
23,000	36,000		< 10	70	
32,000	66,000		< 10	< 10	
67,000	138,000	11	11	10	10

### Start after regeneration



Effluent from Lead Cation filter







## **C – A – (C) versus C - MB**

- C – A – (C) is simpler to regenerate
- C – A – (C) is simpler to automatize
- C – A – (C) gives lower ionic leakage
- C – A – (C) release less organic leachables
- No difference in kinetic properties
- C – A – (C) has slightly higher capital costs
- C – A – (C) has slightly lower operating costs

# Conclusion

**C – A – (C) - superior concept**

- High quality CPP
- Robust and reliable
- Simple automatisation
- Low manpower requirement
- Justified investment